

Synthesis of Highly Oriented Graphite Films with a Low Wrinkle **Density and Near-Millimeter-Scale Lateral Grains**

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ABSTRACT: Principal defects found in graphite films include grain boundaries and wrinkles. These defects are well known to have detrimental effects on properties such as thermal and electrical conductivities as well as mechanical properties. With a two-fold objective of synthesizing graphite films with large single crystal grains and no wrinkles, we have developed a relatively low-temperature (<1150 °C) process that involves the precipitation of graphite films from nickel– carbon solid solutions followed by in-situ etching of the nickel foil substrates with anhydrous chlorine gas to obtain near wrinkle-free continuous graphite films. The size (L_a) distribution of lateral grains (or single crystal regions) in these highly oriented graphite films has been found to be asymmetric with the largest grains about 0.9 mm in diameter, as determined by electron backscatter diffraction (EBSD). Thus, the growth of large-area graphite films with grains much larger than

Type A: Graphite Films from 'Conventional' Synthesis 'Conventional' Synthesis -210.7 nm 33.3 nm 3 nm Type A: T > 1000 °C Ní Wrinkled Films <u>Cool to</u> RT (~20 First Etch Ni with Cl₂ Then Cool to Type B: Near Wrinkle-Free Films RT (~20 °C)

those reported for highly oriented pyrolytic graphite (HOPG, ~ 20 to 30 μ m), and with a low density of wrinkles, as in the case of HOPG, but prepared at much lower temperatures, is reported here.

INTRODUCTION

Methods such as the molten flux route $(>1500 \text{ °C})^{1-5}$ or the metal-carbon solid solution route⁶⁻¹⁷ have been explored to synthesize graphite crystals in the bulk form or as thin films. However, the graphite films generated are often heavily wrinkled, a defect that, along with grain boundaries, dislocations, and vacancies, is largely detrimental to their properties, including thermal and electrical conductivities and mechanical properties. Moreover, although some published studies provide selected area diffraction patterns from transmission electron microscope (TEM) analyses, the analyses are limited to regions $\leq 1 \ \mu m^2$, and none of these studies report the grain sizes of these graphite materials. Another route to synthesizing graphite involves the thermal cracking of hydrocarbons at very high temperatures (>2000 °C) with applied pressure. This process tends to yield nonwrinkled "highly oriented pyrolytic graphite" (HOPG) as products, but the grain sizes are typically limited to ~ 20 to 30 μ m (for grade A HOPG).¹⁸ Another variant of the molten flux method to prepare graphite is the kish-method, where graphite flakes are obtained by the precipitation of C from molten steel. Although these flakes may contain single crystals up to ~ 1 mm in size, they contain iron impurities that must be removed by additional purification.⁴

In this work, we have explored the synthesis of graphite films with minimal wrinkles and large grains by precipitation from Ni-C solid solutions in the temperature range of 1000-1150 °C. The Ni–C solid solution may be considered as a model system to study and control the precipitation of graphite films for the following reasons: (1) the Ni{111} surface is lattice matched to the graphene layers, (2) Ni does not undergo additional reactions (such as phase changes or carbide formation) at our temperatures of interest that could otherwise complicate the process, and (3) C dissolution and segregation and precipitation from Ni have been previously studied in detail by in situ techniques such as LEED and Auger electron spectroscopy by several surface science groups.^{19–23} Methane was selected as the C precursor of choice as it is a thermally stable hydrocarbon that can only be catalytically decomposed in H_2 -rich environments at temperatures <1200 °C: this approach minimizes "soot" or amorphous carbon formation from thermally mediated reactions.

Our typical graphite growth process involved (1) exposure of the Ni foils to CH₄ gas at T_{dissolution} to form Ni–C solutions followed by (2) precipitation of the graphite films at a lower $T_{\text{precipitation}}$ under vacuum and (3) a final cooling step to room temperature (RT) (Process A, Figure 1). Films generated using this process were heavily wrinkled (or buckled), where wrinkles are defined as vertical deviations from a flat surface

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Figure 1. Details of the production of Type A and B films: (i) overall process, (ii) schematic of the process inside the reactor, and, (iii) plots of variation in C solubility with temperature in polycrystalline Ni showing the amounts of C precipitated as graphite during steps 3 (due to a reduction in temperature), and, 4 (due to Ni etching) of the process (ST = step).

(Figure S2). Such films are referred to as Type A films in this manuscript (Figure 2 and Figures S3 and S4). The major cause of the formation of wrinkles in thin films synthesized at high temperatures (>800 °C) is the thermal stress generated due to the mismatch in the coefficients of thermal expansion (CTEs) between the thin film and the growth substrate (other factors such as intrinsic stresses generated during growth and extrinsic stresses due to external factors may also cause wrinkling). For example, when cooled from a growth temperature of 1000 °C to RT, the lattice parameter "a" of face-centered cubic (FCC) Ni changes from 3.58 to 3.52 Å (i.e., ~1.7% contraction),²⁴ while for graphite, the change in the in-plane lattice constant is negligible (Figure S5).^{25,26} This unequal contraction introduces biaxial compressive stresses in the film that are released by forming a network of delamination buckles in the film.

Wrinkling may distort the local crystal symmetry and thus introduce bond strain and crystallographic defects in the graphite film. At a more severe level, wrinkling may even lead to bond breakage in graphite films. Wrinkling has been observed to degrade several material properties in graphene^{27–29} or to enhance its chemical reactivity.^{30,31} Strategies to prevent wrinkling in single-layer graphene include growth on copper substrates with a specific crystallographic orientation (Cu(111)),^{32,33} switching to lower CTE substrates like metallic platinum³⁴ or nonmetallic germanium,³⁵ or growth at lower temperatures (Cu/Ni(111) at 750 °C).³⁶ However, to the best of our knowledge, no attempts on eliminating wrinkling in graphite or multilayer graphene films have been reported in the literature.

RESULTS AND DISCUSSION

Our approach for preventing wrinkle formation in graphite films has been to remove *physical contact* between the Ni foil and the graphite films immediately after growth at 1000 °C and then cool the resulting free-standing graphite films to RT. This essentially involved chemical etching of the Ni foil(s) at $T_{\text{precipitation}}$ or 1000 °C. An ideal reagent for this purpose should have the following characteristics: it should (1) be stable at 1000 °C, (2) have sufficient vapor pressure for easy introduction into a reactor under dynamic gas flow conditions, (3) selectively react with the Ni foil(s), (4) form reaction products with sufficient vapor pressures that can be removed without contaminating the graphite films, (5) not introduce defects into the graphite films, and finally, (6) not interfere with the graphitization process of the dissolved C in the Ni foil(s).

Commercial etchants and aqueous solutions of nonoxidizing and oxidizing acids, such as HCl, HNO₃, H₂SO₄, or H₃PO₄, that are commonly used for etching Ni at temperatures <200 °C cannot be used for high-temperature etching inside a reactor. Oxidizing reagents such as supercritical water or oxygen gas will also completely or partially oxidize the graphite film (and possibly also generate CH_4 , CO_2 , or CO_2) while converting the Ni foil to nickel oxide powder. Similarly, sulfurcontaining etchants such as H₂S acid vapor are known to produce stable S-doped graphene at temperatures above ~600 °C.³⁷ Again, anhydrous HCl or other nonoxidizing acid vapors cannot be used because HCl will produce H₂ gas, both by thermal dissociation ($\sim 0.73\%$ at 1000 °C)³⁸ and upon reaction with Ni, which may etch the graphene layers. Moreover, as the remaining dissolved C in the Ni foil graphitizes as the foil is etched (discussed in detail later), the presence of H_2 may complicate this process by creating vacancies or sp³ carbon. Indeed, H₂-Cl₂ mixtures have been used to form nanodiamond particles or sp³ carbons that are not wanted in our process.39,40

It has been shown that the carbon-halogen bonds in halographenes⁴¹ and graphite fluoride⁴² are unstable at temperatures above 400–700 °C. For example, the C–Cl bond is not stable at high temperatures and pristine graphene can be recovered from chlorinated graphene by heating to temperatures >500 °C.^{43,44} Indeed, one method of purifying natural and kish graphites industrially is by exposing them to anhydrous Cl₂ gas at high temperatures.⁴ Moreover, the synthesis of carbide-derived carbons (CDCs) has been explored with the reaction of carbides MC_x (M = Si, Al, Ti, Zr, V, Nb, Ta, etc.) with Cl₂–Ar under dynamic flow and ambient pressure at ~900 to 1000 °C to form graphitic C and



Figure 2. SEM and AFM images of graphite films. Type A films: (i) SEM image, and, (ii)-(iv) AFM images; Type B films: (v)-(vi) SEM images, and, (vii)-(xii) AFM images. All AFM images show $20 \times 20 \ \mu\text{m}^2$ scan areas. Numbers across the wrinkles denote their heights in nanometers.

 MCl_x .^{45,46} The other halogens react similarly with MC_x and are all potentially suitable agents for etching Ni at high temperatures without damaging the graphite film.^{46,47} Because anhydrous Cl_2 gas has a higher reactivity than Br_2 and I_2 , and because they are respectively a liquid and a solid that would require additional optimization of appropriate bubbler-type set-ups, we selected Cl_2 for the etching process. Fluorine was not selected because of its severe safety hazards.

In order to remove wrinkles, after the graphite films had formed at 1000 °C ($T_{\text{precipitation}}$), anhydrous Cl₂ gas was introduced for ~3 h to etch away the Ni foil sandwiched between the two graphite films that had grown on its two sides

(Process B, Figure 1). The temperature for graphite growth and subsequent Ni etching was selected to be 1000 °C to ensure that the NiCl₂ produced did not contaminate the graphite films because NiCl₂ has a high enough vapor pressure to be removed from the reaction zone under dynamic vacuum.

It is important to note that for the graphite growth runs in which the Ni was etched (process B), the Ni foils were placed in boats with covers to prevent the resulting free-standing graphite films from flying away under this dynamic vacuum (Figure S6). As the Ni etching progressed, an orange anhydrous NiCl₂ powder was deposited on the cooler surfaces of the reactor (Figure S7). When the graphite growth and Ni

etching were completed, the Cl₂ gas was turned off, and the films were cooled to RT after a 5 min wait period at 1000 °C. This wait time was necessary to pump out all the Cl₂ gas before cooling in order to eliminate any possible chance of C-Cl bond formation at lower temperatures (<500 °C). At this point, these graphite films no longer had a Ni substrate in physical contact and hence did not experience the $\sim 1.7\%$ biaxial compressive stress they otherwise would have had. At RT, the films were recovered from the furnace and floated in ethanol or acetone. However, the two graphite films that had grown on the two sides of the Ni foil had collapsed onto each other (with gaps of ~80 to 100 μ m) after the Ni etching process. The films were then separated by gentle mechanical agitation with liquid N₂ (see the Supporting Information for details) and tested for the presence of any metallic Ni(0) residue by bringing a magnet close to them. If the films were not attracted to the magnet, they were tentatively considered free of Ni(0) (Figure S8). The residual Ni concentration was later measured on select films by inductively coupled plasmaoptical emission spectroscopy (ICP-OES). The results given in Table S2 show that the Ni content was quite small, ~ 0 to 1%. The films were then transferred onto silicon wafers and air dried for further characterization. These films are referred to as Type B films in this manuscript.

The surfaces of the Type B graphite films were examined by optical microscopy (Figure S9) and SEM (Figure 2 and Figure S10) and showed a huge reduction in the total number of wrinkles. The films had lost their corrugated appearance, and the larger wrinkles were completely absent. The few remaining wrinkles were possibly caused by mechanical stresses during handling of these free-standing submicrometer-thick films. AFM imaging of the graphite surfaces showed that such wrinkles were ~5 to 20 nm high and ~0.1 to 0.2 μ m wide. AFM imaging also showed that the films were "wavy", as might be expected from such free-standing films. Unsurprisingly, the film had occasional tears or holes, which were most likely a result of mechanical damage during the separation of the two films (Figure 2 and Figure S11).

The etching rate of Ni with Cl₂ was observed to be important for two main reasons. First, etching conditions that were "too harsh" mechanically damaged the films, forming, for example, torn and crumpled films when the Cl₂ flow rate or the reactor pressure were too high (Figure S12). Second, at 1000 °C, the Ni foil not only has graphite films on both surfaces but also about 1.3 at. % C in the bulk (Figure 1). This dissolved C graphitizes during the Ni etching step (neither the dissolved C nor the precipitated graphite are etched by Cl₂ at this temperature, as explained earlier). This suggests that the Ni etching rate may be an important parameter to consider to better control the C precipitation during Ni removal and the final structure of the graphite films. Hence, in order to form large graphite grains, the etching must be carried out at an optimized rate so that these C atoms are added to existing grains instead of randomly nucleating smaller new ones. Although we were able to optimize the etching rates so that minimally damaged films with large grains were produced, we were not able to independently evaluate the effects of rapid etching on the grain size, because this forms crumpled graphite films that could not be characterized by the diffraction techniques to be discussed later.

Graphite growth in process B thus occurs in two stages: (1) by nonisothermal precipitation as a result of a reduction in temperature from $T_{\text{dissolution}}$ to $T_{\text{precipitation}}$ (step 3, Figure 1),

and (2) by isothermal precipitation at $T_{\text{precipitation}}$ as the amount of Ni is reduced by chemical etching (thus continuously saturating the Ni with C; step 4, Figure 1). No obvious difference in quality was observed between the graphite precipitated in steps 3 and 4 (see Supporting Information for details). As a consequence of this Ni etching step, Type B films were found to be much thicker than the films grown without Ni etching, as performed for Type A films. Thus, Type B films have an average thickness in the range of ~750 to 800 nm, while Type A films have an average thickness of ~250 nm (Figure S13), values that approximately match the predicted thickness from C solubilities (Predicted: Type B, 805 nm; Type A, 265 nm; Table S1).

The initial characterization of the chemical nature of the assynthesized films included electron energy loss spectroscopy (EELS), X-ray photoelectron spectroscopy (XPS) analysis, and Raman spectroscopy. EELS and XPS analyses showed that the film contained only sp² carbon and that no additional functionalization was present (Figures S14 and S32). Raman mapping was performed on several samples to obtain information on the film quality from the I_D/I_G ratio, and it ranged from ~0.04 to 0.09 (Figure S15, Table S3-i), indicating that they were high quality with mostly sp²-bonded C atoms.

In order to determine the stacking order of the graphene layers, Raman mapping of the 2D peak was performed, and the stacking order was evaluated based on the method of Cancado et al. (see the Supporting Information for details).⁴⁸ For a Grade A HOPG sample with almost complete AB stacking, the metric obtained by this method was ~1.0, whereas for both Type A and Type B films, it varied from ~0.84 to 1.0 (Table S3-ii). However, our films did show regions, where the AB stacking order is obviously broken (Figure S17), but at this time, we are not certain what causes such disorder and hypothesize that such regions may be due to defects such as stacking faults or grain boundaries. These Raman results are consistent with the XRD data (discussed later) from which an "average" d_{0002} spacing of 3.35 Å was obtained for all samples, which also implies that the layers are mostly AB stacked.

The crystal dimensions in both the "a" $(L_a \text{ or lateral})$ dimensions) and "c" directions (L_c) must be determined to define the size of a single crystal or grain in our films, and electron backscatter diffraction (EBSD) has been used to determine the orientation and lateral grain size of the films. EBSD is a common technique for the determination of orientation and grain size in metallic and ceramic samples that utilizes Kikuchi patterns produced by backscattering of diffusely scattered electrons inside the sample for phase identification and determination of the crystal orientation. EBSD analysis has been used for characterizing graphitic regions in iron^{49,50} and has been reported for graphite samples in two conference proceedings.^{51,52} To the best of our knowledge, there has been no earlier work on the use of EBSD to obtain a detailed and rigorous evaluation of the grain orientation and size in graphite.

In order to verify that EBSD can be used to determine the graphite grain orientation and size, EBSD was first performed on flakes of natural graphite transferred to silicon wafers. In EBSD, the software utilizes a user-defined sample co-ordinate system and phase to match the Kikuchi bands of the sample with reference patterns and determines crystal orientation.⁵³ Thus, one relatively stringent requirement is that the sample surface must be completely flat and perpendicular to the normal direction (ND) of the sample co-ordinate system at all

points. Hence, all samples were pressed with a roller a few times before measurement, which may have introduced additional wrinkles. Because graphite is a soft and layered material, no other chemo-mechanical polishing that is common for the preparation for metallic and ceramic samples for such studies was performed as it could have severely damaged the surface.

Orientation mapping involves the determination of the crystal orientation (or index) of all pixels in a scan and then delineating grain boundaries based on the mis-orientation between these pixels. Hence, the first step after collecting the scan from a natural graphite flake was to evaluate the quality of the Kikuchi patterns obtained using an image quality (IQ) map (Figure S18-i) followed by the evaluation of the confidence index (CI) map that shows the CI values associated with each pixel. The CI values represent the acceptability of the indexing results and range from 0 to 1 (Figure S18-ii). Only orientations with CI values >0.1 were considered for subsequent analysis after processing (Figure S18-iii). Finally, the indexing success rate (ISR) was determined, where ISR is simply the ratio of the points with CI values >0.1 to the total number of scanned points. As shown in Figure S18, there is good correlation between the IQ and CI maps, and the ISR is ~99.6%, indicating that this is a good scan. The details of this process have been provided in the Supporting Information.

The EBSD data may be represented by pole figures (PFs), inverse pole figures (IPFs), IPF maps, and kernel average misorientation (KAM) maps. The PFs show plots of specified crystal directions or poles of the different unit cells of the grains in the sample with respect to the sample coordinate system. On the other hand, IPFs show plots of a sample direction (such as the ND) with respect to specific crystal directions of the differently oriented unit cells in the sample. Thus, two key pieces of information are obtained simultaneously: the number or set of points reflects the number of grains in the sample, whereas their locations indicate the location of specific crystal directions of the different grains (i.e., single crystal regions) with respect to the sample co-ordinate system. In both the PFs and IPFs, the points have been weighted by the associated grain sizes for easy identification of a particularly large grain and multiple smaller grains, as is often the case. Figure S19-I-i shows the plots of the PFs for the (0001) and $(10\overline{11})$ crystal directions of the different grains in the scan for natural graphite. It contains two large points (for the (0001) PF) or sets of points (for the $(10\overline{1}1)$ PF) and several tiny (or sets of tiny) points, which implies that the scanned region contains two large grains. The IPF for the natural graphite scan (Figure S19-I-ii) shows the plots of the sample ND with respect to the crystal directions of the different grains. It contains points close to the (0001)direction, implying that the (0001) directions of the different grains are essentially parallel to the sample ND. In other words, the {0001} planes of all grains in the film are parallel to the sample surface. The IPF also shows two coincident large points, implying that two large grains are present. Finally, the IPF map is color coded to represent the orientation of the ND of each pixel in the scan, which for this scan is parallel to the (0001) directions of all associated grains (Figure S19-III). The last step of the EBSD scan analysis involves delineating the grain boundaries and calculating the grain size (see Supporting Information). The grain diameters for regions 1 and 2 have been calculated from their areas to be ~500 and ~450 μ m, respectively. Figure S19-IV shows the KAM map from the

natural graphite scan comparing the mis-orientation between neighboring pixels: the mis-orientation between the first nearest neighbors is generally $<2^{\circ}$.

Several Type B films have been analyzed by EBSD. However, perhaps because of an uneven surface topography, the ISR values were somewhat lower. Smaller scan areas ($\leq 125 \times 200 \ \mu$ m) tended to have larger ISR values (~99%), but the grain sizes were artificially limited by the areas scanned (Figure 3 and Figures S20 and S21 and Table S4). To determine the



Figure 3. EBSD scans of **Type B** graphite films. (I) A high resolution scan with a step size of 250 nm, and, (II) A scan where the grain size is limited by the scan size: (i) IPF map of the sample ND (Scale bars: 5 μ m (I), 50 μ m (II)); (ii) IPF of the sample ND; (iii) left: (0001) PF, and, right: (1011) PF. Grain boundaries are represented in white and black areas represent pixels with CI < 0.1 that have not been included in the IPF maps. The points in the PFs and IPFs have been weighted by grain size. ND refers to the normal or (001) direction of the sample co-ordinate system.

"true" grain sizes, EBSD scans over an area of about 1.5×1.5 mm² were performed. Figure 4 shows the IPF and PF plots for two Type B films with the {0001} orientation and the largest grains about 0.9 mm in diameter. The (0001) PFs for both films show a single large point, and the (1011) PFs show one set of large points, confirming that these regions are single crystals. The yellow regions in the IPF map and the circled points in the PFs and the IPFs are from the exposed silicon wafer where the films have holes or tears (Figure S27). A large area scan from a Type A-wrinkled film is shown in Figure S23 and shows that the largest grain diameter is about 0.8 mm. The KAM maps and details of all large area scans are provided in Figure S22 and Table S5.

A probable reason for the lower ISRs can be obtained by comparing the maps in Figure S24, where the SEM image (i), the "raw" IQ map (ii) and the IQ (iii) and the CI (iv) maps from postprocessing are shown. From these figures, it is obvious that nonflat regions have lower IQ values that result in low CI values and poor indexing. In this example, the nonflat regions are the ones where the film has torn materials deposited on top of it, which perhaps obscure the Kikuchi patterns from the film lying beneath it. However, even without material deposition on the top and a sharp Kikuchi pattern, the local surface curvature (i.e., any deviation from the user defined sample co-ordinate system) may result in a failure by the software to index the pixel with an acceptable CI value and lead to an overall lower ISR for the scan.

Figure 5 shows a comparison between similar area scans from a Type B film, a natural graphite flake, and commercial grade A HOPG. It is concluded from the unique grain color maps that grain sizes in grade A HOPG are much smaller (6– 26 μ m) than in the natural or Type B graphite samples. Again,



Figure 4. Large area EBSD scans of two **Type B** graphite films (I) and (II): (i) IPF map for the sample ND; (ii) IPF map for the sample ND with the largest grain highlighted in gray (Scale bars: (I) 600 μ m; (II) 500 μ m); (iii) left: (0001) PF, and, right: (1011) PF; (iv) IPF of the sample ND; (v) grain size chart with the largest grain highlighted in gray. Grain boundaries are represented in white and black areas represent pixels with CI < 0.1 that have not been included in the IPF maps. Yellow regions in the IPF maps or the points circled in yellow on the IPFs and PFs are from the bare silicon wafer. The points in the PFs and IPFs have been weighted by grain size. ND refers to the normal or (001) direction of the sample coordinate system.

the quasi ring-like appearance of the $(10\overline{11})$ PF of grade A HOPG versus the single set of large points for natural graphite or the Type B graphite film clearly demonstrates that the grains in HOPG are much smaller.

XRD experiments that involved coupled ω -2 θ scans with a 0-D detector were performed to probe the crystal structure in the "c" direction and showed that the films have a preferred orientation because only the {0002} family of peaks was detected. The d_{0002} values calculated from these scans were all clustered around 3.354 Å (Table S7-i), which implies that the films are, on average, AB stacked (a higher d_{0002} value would imply turbostratic stacking).⁵⁴ This result does not contradict the Raman spectroscopic analysis discussed earlier showing occasional deviations from AB stacking. This is because Raman spectroscopy has a much higher resolution (spot size of beam ~700 to 800 nm at 100× magnification; information depth ~30 nm), whereas XRD provides an average value for the

entire film (spot size of beam ~ 1 mm; information depth \sim entire film).

Mosaic spread is a parameter that is commonly used for HOPG samples to determine crystallite (or single crystal) alignment in the "c" direction and a lower value of this metric signifies greater crystallite alignment (see the Supporting Information for details). The mosaic spread values obtained were in the range of ~0.1 to 0.2° for Type B films and ~0.5° for Type A films. This indicates that the crystallite alignment in Type B films is at least as good as in Grade A HOPG, keeping in mind that these films are not perfectly flat which may artificially increase the mosaic spread value.

High-resolution TEM (HR-TEM) was also used to study and compare Type A and Type B graphite films (Figure 6). Electron transparent Type A films imaged in the top-down mode (plan view TEM) showed a heavily wrinkled appearance with 3-4 wrinkles often emerging from common junction



Figure 5. Comparison of similar sized EBSD scans (~125 × 220 μ m²): (I) Type B graphite film, (II) Natural graphite flake, (III) Grade A HOPG (Optigraph); (i) the IPF map for the normal direction of the sample co-ordinate system; (ii) the unique grain color map; (iii) left: (0001) PF, and, right: (1011) PF for the respective scans. Scale bars for (i) and (ii): 50 μ m. Grain boundaries are represented in white (IPF map) or gray (unique grain color map) and black areas represent pixels with CI < 0.1 that have not been included. The points in the PFs have been weighted by grain size.



Figure 6. HR-TEM images and selected area diffraction (SAED) patterns of graphite films. **Type A** films: (i) a wrinkle junction; (ii) SAED patterns from a region containing a wrinkle junction (P: junction point) where spots adjacent to the stars are examples of select "additional" spots in the patterns from wrinkles W1, W2 and P; R: region; (iii) defect-free crystal lattice; (iv) (1) lower and (2) higher magnification images of a region containing a conformal bend, and, digital diffractograms (right) from selected regions showing variation in crystallinity; (v) (1) lower and (2) higher magnification images of a region containing a conformal bend, and, digital diffractograms (right) from selected regions showing variation in crystallinity; (v) (1) lower and (2) higher magnification images of a region containing a nano-buckle with the spacing of the d_{0002} lattice fringes in regions 1–3 tabulated below. **Type B** films: (vi) image, and, (vii) SAED pattern from a film thinned to electron transparency; (viii) cross-section image, and (ix) SAED pattern of a typical ~800 nm film.

points. High-magnification images of these junction regions revealed "gaps" where the graphene layers had physically separated, possibly due to shear stress. Selected area electron

diffraction (SAED) of such junctions was then done to explore whether wrinkling had locally modified the orientation. SAED showed no change in orientation although additional diffraction spots were present, possibly from the folded over part in the wrinkle. On the other hand, cross-sectional TEM imaging performed on thicker and thinner Type A films revealed two types of large angular bends $(>100^{\circ})$ in the {0002} lattice fringes of the graphene layers. These include ~130 to 160° conformal bends adjacent to the Ni substrate and ~ 130 to 150° nanobuckles within the graphene layers of the film. Nanobuckles may show variations in the d_{0002} lattice fringe spacing and may have adjacent physical gaps. Both nanobuckles and conformal bends may have neighboring regions of lower crystallinity. The details of the TEM characterization of Type A-wrinkled films and the possible implication of buckling of the graphene layers on the growth process and film properties will be reported elsewhere.

For Type B films, the plan-view HR-TEM image on a film thinned to electron transparency by mechanical exfoliation showed the region to be a single crystal with AB stacking. Figure 6-viii,ix show the cross-section of a Type B film and respectively a high-resolution image and a diffraction pattern, proving that it is a highly crystalline material. Again, the sharpness of the diffraction spots indicates that this is a singlecrystal region.

In order to further understand the role of the Ni substrate on graphite grain size, attempts were made to correlate the grain structure of the Ni substrate with that of the graphite film. It was found that considerable grain growth had occurred in the Ni foil after the H_2 pretreatment step (step 1, Figure 1) and that the foil contained grains of different orientations that could be as large as ~850 μ m (Figure S29). The fact that the largest graphite grains were also ~800 to 900 μm in size suggests that a relationship may exist between the grain sizes of the graphite film and the Ni substrate. Again, the graphite grains were always found to have the {0001} orientation. Thus, the graphene layers of the films grow parallel to the Ni substrate irrespective of the orientation of the Ni grains. This has been previously observed by Johansson et al. while exploring the orientations of their graphite films and the underlying polycrystalline Ni substrate by electron diffraction in the TEM.⁵⁵ Additional details on the role of the substrate on graphite film growth will be reported elsewhere.

One of the major improvements expected from the removal of wrinkles in graphite films is a significant increase in their Young's modulus/ stiffness. Hence, removing wrinkles from an area fraction = 0.1, from films that have wrinkle amplitude/film thickness ratios ranging from 1 to 10, would increase their respective Young's modulus by a factor of 0.6-60.⁵⁶ However, the removal of wrinkles is not expected to significantly influence the film strength and the potential applications for wrinkle-free graphite films are where "high-modulus carbon films" are required (similar to high-modulus carbon fibers that are obtained by the removal of the misalignment between the constituent crystalline carbon ribbons).

On the other hand, removal of grain boundaries is expected to increase the film strength and stiffness.^{57,58} An increase in grain size has been observed in silico as capable of increasing the fracture strength of polycrystalline graphene, following an inverse Hall–Petch-like relation and demonstrating that the grain boundary junctions are the weakest links. From this result, a ~2 times increase in strength may be expected with an increase in grain size *d* in a graphite film of a size *L*, when the L/d ratio changes from 10,000 to 10. Accordingly, the potential applications for both wrinkle and grain boundary-free graphite films are where "high-modulus and high-strength carbon films" are required. A detailed discussion can be found in the Supporting Information.

CONCLUSIONS

We have shown that we can grow graphite films with few wrinkles by growing them on Ni foils at high temperatures and then removing the Ni substrates by chemical etching to eliminate issues caused by the CTE differences between the films and the foils. Moreover, by optimizing the process parameters, we have grown continuous graphite films with near-millimeter-scale lateral grains. We believe that this is the first report of an attempt to reduce wrinkling in thin films of a layered material, with single-layer graphene being a notable exception. This is also the first rigorous attempt to unambiguously determine grain sizes in graphite by EBSD, which has been used extensively for this purpose. Initial calculations on mechanical properties predict a significant improvement in axial stiffness and strength in these films attributed to a reduction in the number of wrinkles and an increase in grain size.

However, intrinsic stresses from the growth process and external stresses generated after the growth process that may cause other defects including fine wrinkles have not been eliminated or studied. The current technical limitations of the overall process include the formation of holes or tears in the films and the inability to obtain pristine thin films of graphite or multilayer graphene, both due to the difficulty of handling such free-standing films in the reactor without mechanical damage. Such limitations may be removed with appropriate equipment and experimental design modifications, such as by using more suitable sample holders. In the future, we hope to see such films generated so that the expected property improvements discussed above can be studied and evaluated.

EXPERIMENTAL SECTION

In a typical process, the reactor was loaded with $\sim 1 \text{ cm}^2$ pieces of Ni foil (thickness: 100 μ m; purity: 99.994%, metals basis) in quartz boats covered with alumina lids. The furnace temperature was slowly increased to 1150 °C in 1 h 15 min (~15 °C/min) under an Ar/H₂ flow at 100 Torr followed by a 15 min hold at 1150 °C (step 1). This was followed by a CH₄ exposure step at a pressure of <0.1 Torr (step 2). Then, all gases were turned off and the temperature was quickly reduced to 1000 °C (at 10 °C/min) and held at 1000 °C for 1 h under dynamic vacuum to precipitate the graphite films (step 3). This quick temperature reduction was to minimize graphite precipitation during this ramp down process and ensure that most of the film is generated at 1000 °C. In one set of experiments (Process A, Figure 1), the samples were then fast cooled to RT by switching off and sliding the furnace ~ 20 cm away from the samples and turning on a table fan. Finally, the Ni foils with graphite films on both sides were recovered. Selected films were delaminated using the electrochemical delamination method⁵⁹ with ~1 M NaOH after (spin)coating them with polymeric PMMA (polymethyl methacrylate) support layers. These graphite-PMMA films were transferred to silicon wafers or other substrates of choice followed by PMMA removal using acetone and H₂/Ar treatments at 400 °C.

In a second set of experiments (Process B, Figure 1), after the formation of the graphite films at 1000 °C, ~10 to 20 sccm of anhydrous Cl_2 gas was introduced into the reactor for ~3 h (step 4). At the end of this process, the Cl_2 gas was turned off, and after a 5 min wait time, the furnace was turned off and cooled to RT (step 5). At the end of this process, *only* unsupported graphite films were

recovered. The graphite films were then collected and floated in ethanol or acetone. At this point, each recovered film was composed of two graphite films ("collapsed" films) that had originally grown on the two sides of each Ni foil and collapsed onto each other during the Ni etching. Liquid N_2 was added slowly to the ethanol where the films were floating, and these two graphite films were separated by gentle mechanical agitation. The films were then transferred to substrates of choice for further characterization.

Additional experimental details including characterization methods can be found in the Supporting Information.

ASSOCIATED CONTENT

Supporting Information

The Supporting Information is available free of charge at https://pubs.acs.org/doi/10.1021/acs.chemmater.0c00154.

Details of synthetic and characterization methods and mechanical property calculations; and profilometry data, XPS spectra, EELS spectra, Raman spectra, XRD data, and additional optical microscopy, SEM and AFM images, and EBSD scans (PDF)

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Notes

The authors declare no competing financial interest.

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Supporting Information

Synthesis of Highly Oriented Graphite Films with a Low Wrinkle Density and Near-Millimeter Scale Lateral Grains

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Experimental Details

<u>Materials</u>

Nickel foils of different thicknesses and purities were purchased from Alfa-Aesar (100 µm thickness and 99.994% purity; 25 µm thickness and 99.99% purity). Natural graphite crystals were obtained from Prof. John Jaszczak (Michigan Technological University & Naturally Graphite). Grade-A and Grade-B HOPG were purchased from SPI (USA), XFNano (China) and Optigraph (Germany). Ultrahigh purity grade (99.999%) CH₄, H₂, and Ar gases were used for all graphite growth processes. The gases were additionally purified using respective purifiers before use. Anhydrous Cl₂ gas (99.999%) was used as received.

Characterization

AFM was performed on a Bruker Dimension Icon system. SEM imaging was performed on a Verios 460 scanning electron microscope and EBSD scans were obtained using a Hikari camera from Ametek attached to this SEM. TEM images and EELS spectra were recorded on a probe corrected FEI Titan G2 60-300 instrument with an electron monochromator at 80 kV. XRD data was obtained on a Rigaku SmartLab powder X-ray diffractometer. Confocal Raman spectroscopy was performed on a WiTEC instrument using a 532 nm laser and 600 g/mm or 1800 g/mm gratings. XPS measurements were acquired on a Thermo Scientific ESCALAB 250 Xi instrument. ICP-OES data was acquired on a Varian 700-ES instrument.

Sample Preparation for EBSD

Flakes were extracted from natural graphite crystals or HOPG pieces by pressing them to sticky notes followed by removal of the adhesive sticky notes with HPLC grade acetone. The free-floating pieces were then transferred to silicon wafers and dried in an oven at 80–100 °C. All the natural graphite or HOPG flakes thus obtained and Type A and Type B graphite films on silicon wafers were pressed a few times using a Kolami 330 S roller prior to performing EBSD scans.

Sample Preparation for Cross-section TEM

Regions of interest (ROI) from selected graphite films on Si wafers or Ni substrates were first coated with a Ti film and then with a black marker pen outside the SEM chamber. Once inside the SEM chamber (Helios 450HP) the ROI was coated with amorphous carbon and then sectioned with a focused ion beam (FIB) of gallium ions at 30 kV, and at an angle of $\pm 2^{\circ}$ to the surface normal. After transferring this wedge to a half grid, the final milling was also done with a gallium FIB sequentially at 30 kV, 5 kV and 2 kV and *without tilting*. This procedure has been adopted from a previous study by Colby et. al. to minimize ion beam damage to the graphite film.¹



Figure S1. Figure representing a cross-section sample prepared from a graphite film for TEM imaging.

<u>**Table S1**</u>. Predicted number of graphene layers precipitated on each side of a 100 μ m Ni foil, based on thermodynamic solubility data for C in polycrystalline Ni,² from a T_{dissolution} temperature of 1150 °C. The calculation is based on the C solubility difference between T_{dissolution} and T_{precipitation}.

Number of graphene layers

= (C solubility difference T_{dissolution} and T_{precipitation})*(Ni thickness)* unit cell area/ # of atoms per unit cell

where, unit cell area = $3\sqrt{3}/2*a^{2}$, and, atoms per unit cell = 2, for each graphene layer.

For a 100 µm Ni foil, it has been assumed that half the excess carbon precipitates on each side, hence,

thickness = $50 \,\mu m$.

Film thickness = Number of graphene layers (0.335 nm)

T _{precipitation} (°C)	Number of graphene layers	Film Thickness (nm)
20 (RT)	2405.359456	805.7954177
600	2118.984173	709.8596978
650	2019.596995	676.5649932
700	1901.359476	636.9554246
750	1763.831489	590.8835488
800	1606.886348	538.3069267
850	1430.667738	479.2736922
900	1235.545145	413.9076235
950	1022.070829	342.3937277
1000	790.9401518	264.9649508
1050	542.9562114	181.8903308
1100	278.9991366	93.46471075

Thus, the maximum predicted film thickness is ~806 nm; this should be compared to Type B films. Type

A films precipitated at 1000 °C are expected to have thicknesses around ~265 nm.

AFM analysis of wrinkles

Figure S2 depicts what has been defined as the height of a wrinkle and how it has been measured using AFM. Generally, AFM analysis is performed on the side that was away from the Ni substrate during growth (outer side, **Figure S3**). However, select films have been flipped over and AFM has been performed on the side that was adjacent to the Ni surface (inner side). They show similar wrinkling patterns (**Figure S4**).



Figure S2. AFM analysis showing wrinkles on a graphite thin film characterized by their height H, length L and width w: (i) image, (ii) a typical line scan.



Figure S3. AFM analysis of Type A film on their 'outer' side. Numbers across the wrinkles represent their heights in nm. Scan areas: (i)-(ii), (iv): $20x20 \ \mu m^2$; (iii), (v): $5x5 \ \mu m^2$.



Figure S4. AFM analysis of Type A film on their 'inner' side. Numbers across the wrinkles represent their heights in nm. Scan areas: (i): $40x40 \ \mu m^2$; (ii): $20x20 \ \mu m^2$



Figure S5. Variation in lattice parameters of (i) Ni, and, (ii) Graphite, with temperature. For face centered cubic (FCC) Ni this is the lattice parameter 'a' of its cubic unit cell, whereas, for graphite, this is the inplane lattice parameter.³⁻⁵



Figure S6. (i) Picture of Ni foils on quartz boats and alumina covers loaded in the reactor for synthesizing graphite films. (ii) (a)-(b) Graphite films that have flown away from the center to other parts of the reactor, from an experiment without protective lids.



Figure S7. (i) Orange anhydrous NiCl₂ deposited on the cooler surfaces of the reactor (~500-600 °C).
(ii) Raman spectrum of anhydrous NiCl₂.⁶

Evaluating the amount of Ni(0) or NiCl₂ in Type B films

<u>Magnet Test</u>: At the end of an experiment, a magnet was brought close to a floating Type B film. If the film was not attracted by the magnet, it was tentatively considered to contain an insignificant amount of Ni(0) (**Figure S8**) residue.

Table S2. ICP-OES Data

Sample#	Magnet Test	ICP-OES: Ni (% by weight)
2-9-18	No Ni(0)	-0.12
2-8-18	No Ni(0)	-0.0013
2-25-19	No Ni(0)	1.01
2-6-18	Ni(0) present	98
2-5-19	Ni(0) present	38
3-16-19	Ni(0) present	89



Figure S8. (i) A Type B graphite film floating in ethanol that is not attracted to the magnets indicating that it has an insignificant amount of metallic Ni(0) residue. (ii) A partially etched Ni-graphite sandwich: the core looks Ni rich while the edges look graphite like.



Figure S9. Optical images of Type B graphite films. Scale bars: $20 \ \mu m$ (i, iii); $50 \ \mu m$ (ii, iv).



Figure S10. Additional SEM images of Type B graphite films. Scale bars: (i) 500 μm, (ii) 100 μm, (iii) 20 μm, (iv) 5 μm.



Figure S11. Additional AFM scans of Type B graphite films: (i), (iv): $40x40 \ \mu m^2$, (ii)-(iii), (v), (vii) - (viii): $20x20 \ \mu m^2$, (ix): $15x15 \ \mu m^2$, (vi), (x): $10x10 \ \mu m^2$, (xi): $2x2 \ \mu m^2$. Numbers across the wrinkles denote their heights in nm.



Figure S12. Damaged and crumpled graphite films formed by un-optimized Cl_2 etching: (i) – (ii) are optical images; (iii) – (iv) show SEM images of films with significant crumpling. Scale bars: (iii) 400 µm, (iv) 50 µm.



Figure S13-I. (i) Typical surface profilometry scans of a (i) Type A, and a (ii)-(iii) Type B graphite films. Heights are in Å. The thicknesses are similar to the calculated thicknesses in **Table S1**.



Figure S13-II. XPS depth profile for C in a Ni foil from **process A** (after graphite films have been removed), showing the presence of atomic C in the bulk. The Ni foil was etched with an argon ion beam and XPS signals were collected after each etching step. The above figure shows XPS spectra from the surface (0 s etching), and after etching for 120 s, 360 s and 4680 s.



Figure S14. Typical XPS spectrum of a Type B graphite film confirming the presence of only sp² C in the film. (i) Survey spectrum, (ii) C1s peak.

Raman Spectroscopy of Graphite Films and HOPG

<u>Table S3-(i)</u>: G peak fitting and calculation of I_D/I_G ratios over the areas scanned (~100–2x10⁴ µm²).

Raman maps were recorded using a 532 nm laser at ~2–25 mW power and a 600 g/mm grating.

Sample Details	I _D /I _G : Average (Median)	G: Average (Median)/cm ⁻¹	FWHM: Average (Median)/cm ⁻¹
HOPG-A	0.02 (0.017)	1583 (1583)	15.48(15.28)
(XFNANO)			
Sample 1 (Type A,	0.12(0.082)	1580(1580)	15(15)
wrinkled)			
Sample 1 (Type B)	0.04 (0.035)	1587(1587)	15(15)
Sample 2 (Type B)	0.06 (0.057)	1581(1581)	15.7(15.4)
Sample 3 (Type B)	0.09(0.07)	1583(1583)	15.19(14.97)
Sample 4 (Type B)	0.06(0.04)	1579(1579)	14.29(14.13)



Figure S15. I_D/I_G maps for (i, ii) two different Type B films (100x100 μ m²).

A method by Cancado et al. has been used to determine the AB stacking order from the 2D peak.⁷ Briefly, this involved fitting the 2D peaks with a 2D₁ peak at ~2714 cm⁻¹, a 2D₂ peak at ~2670 cm⁻¹ and a 2D_T peak (T: turbostratic peak) at ~2698 cm⁻¹ (**Figure S16**). The AB stacking order over the scanned area was then calculated as the ratio of the area of the 2D₂ peak to the sum of the areas of the 2D₂ and 2D_T peaks and compared to HOPG. For a Grade A HOPG sample with near complete AB stacking of the graphene layers, this 2D area ratio was ~1.0. Hence, scanned areas from the graphite films that had an area ratio equal or close to 1 were considered to be AB stacked. <u>**Table S3-(ii)</u>**: 2D peak fitting and calculation of percentage of AB stacking over the areas scanned (~100 μ m²). Raman maps were recorded using a 532 nm laser at ~25–30 mW power, a 100x objective lens and a 1800 g/mm grating.</u>

		D ₁ : Average (median)/cm ⁻¹	D ₂ : Average (median)/cm ⁻¹	DT: Average (median)/cm ⁻¹	Areas ratios of D ₁ /(D _T + D ₁): Average (median)
HOPG-A (XFNANO)		2714(2714)	2671(2672)	2697(2696)	1.0(1.0)
Sample A (Type B)	4	2713(2714)	2669(2669)	2698(2698)	1.01(1.02)
Sample B(Type B)		2715(2715)	2672(2672)	2698(2700)	1.0(1.0)
Sample C(Type B)		2715(2715)	2671(2671)	2697(2695)	0.98(0.99)
Sample (Type A wrinkled)	1	2715(2716)	2671(2672)	2696(2695)	0.96(0.97)



Figure S16. An example of a 2D peak from a Type B graphite film being fitted with a $2D_1$, a $2D_2$ and a $2D_T$ peak. As the area under the $2D_2$ peak is negligible, the graphite film at this point may be considered to be AB stacked.



Figure S17. Examples of Raman spectra showing turbostratic character where, G1 denotes a 600 g/mm grating and G2 denotes a 1800 g/mm grating. The 2D peaks were recorded with the higher resolution G2 for clarity.

EBSD Analysis of Graphite Films

EBSD scans were typically performed using a 6.4 nA current and at 20 kV with the sample surface tilted by 70° and using a hexagonal sampling grid. Step sizes for the maps ranged from $0.25 - 25 \mu m$. The standard post-processing steps included confidence index (CI) standardization (where the low CI of a point was replaced by the higher CI value of a neighboring point with the same orientation) followed by the creation of a partition that excluded points with CI < 0.1. Finally, the grain tolerance angle and minimum size were defined before the different plots and charts were generated.

As explained by Demirel et. al.,⁸ EBSD scans have an inherent instrumental broadening that typically has a FWHM of ~1°, and grain tolerance angles $\geq 2^{\circ}$ should be used to define mis-orientations. It was also reported by Demirel et. al. that this dispersion in orientation increases monotonically with increasing scan size (for single crystal silicon). Finally, variability in mounting and tilting of the sample that may locally change the geometry of the incident beam will cause orientation variability across the scan. This last type of topographic variation is quite common for the millimeter scale scans of the graphite films, as their surfaces are not perfectly flat. Additionally, the films sometimes have loose graphitic material deposited on the surface possibly from the torn regions of the film: it is hard to get good quality Kikuchi patterns or acceptable indexing from such areas. Thus, a grain tolerance angle of 2° and minimum size of 2 pixels have been used to define grains unless mentioned otherwise. Grain areas have been determined by multiplying the area of each hexagonal pixel by the number of pixels included in the grain. Grain diameters have been calculated as the diameter of circles occupying equivalent areas. It should be noted here that using a grain tolerance angle of 5° (ASTM protocol E2627) often produces an increase in grain size and the largest grain diameters thus obtained may be as large as ~1.4 mm (Figure S25). Hence, by using a tolerance angle of 2°, we have provided a somewhat conservative estimate of the grain size. In all PFs and IPFs, the points have been weighted by associated grain sizes. In all figures, the IPFs and the IPF maps are with respect to the sample normal direction. KAM maps have been plotted using the 1st nearest neighbors and an upper limit of 5°.



Figure S18. Image Quality (IQ) map from raw data (i), and, Confidence Index (CI) maps obtained from raw data (ii) and, after processing (iii) from an EBSD scan of a natural graphite flake. Black areas in (iii) have CI < 0.1.



Figure S19. Large area EBSD scan of a natural graphite flake: (I) (i) (0001) and ($10\overline{1}1$) PFs, and, (ii) IPF from the entire scan; (II) (i) (0001) and ($10\overline{1}1$) PFs, and, (ii) IPFs from regions 1 and 2; (III) IPF map for entire scan; (IV) KAM map for entire scan. Black areas represent pixels with CI < 0.1 that have not been included and grain boundaries are represented in white in the IPF and KAM maps. The points in the PFs and IPFs have been weighted by grain size. For this scan, ISR = 99.6% and the step size used = 4 µm. All IPFs and IPF maps are of the sample normal direction (001).



Figure S20. KAM maps for the 'smaller' EBSD scans in (I) Figure 3-I, and, (II) Figure 3-II. Black areas represent pixels with CI < 0.1 that have not been included and grain boundaries are represented in white.



Figure S21. (i) IPF map of a ~0.13x0.2 mm² scan; (ii) IPF map, (iii) KAM map, (iv) (0001) and ($10\overline{1}1$) PFs, and, (v) IPF of a cropped 'single-crystal' area 1. Black areas represent pixels with CI < 0.1 that have not been included and grain boundaries are represented in white in the IPF and KAM maps. The points in the PFs and IPFs have been weighted by grain size. All IPFs and IPF maps are of the sample normal direction (001).

Sample Details	Step size	ISR (%)	Largest grain size	
	(µm)		Diameter (µm)	Area (µm ²)
Fig. 3-I	0.25	99.7	28	619
Fig. 3-II	2	99.8	189	28672
Fig. S21	1.5	99.4	174	24332

Table S4: Details of 'small' EBSD scans

Figure S22. KAM maps for the 'larger' EBSD scans in (i) Figure 4-I, and, (ii) Figure 4-II. Black areas represent pixels with CI < 0.1 that have not been included and grain boundaries are represented in white.

Sample Details	Step size	ISR (%)	Largest grain size	
	(µm)		Diameter (µm)	Area (mm ²)
Type B (Fig. 4-I)	20	80	904	0.62
Type B	20	80	877	0.62
(Fig. 4-II)				
Type A	10	73	826	0.56
(Fig. S23)				

Table S5: Details of large EBSD scans

Figure S23. EBSD scan of a Type A graphite film: (i) IPF map, (ii) IPF map with the largest grain highlighted in gray, (iii) KAM map, (iv) Grain size chart, (v) (0001) and ($10\overline{1}1$) PFs, and, (vi) IPF. Grain boundaries are represented in white, black areas represent pixels with CI < 0.1 that have not been included and yellow regions are from the bare silicon wafer in the IPF and KAM maps. The points in the PFs and IPFs have been weighted by grain size. All IPFs and IPF maps are of the sample normal direction (001).

Figure S24. (i) SEM image, (ii) Raw IQ map, (iii) – (iv) IQ map and IPF map obtained from postprocessing. Black areas represent pixels with CI < 0.1 that have not been included in (III)-(IV) and grain boundaries are represented in white in (IV). All IPFs and IPF maps are of the sample normal direction (001).

Figure S25. Grain size estimation with a tolerance angle of 5° for the EBSD scan of a Type B film in **Figure 4-B**: (I) IPF map, (II) IPF map with the largest grain highlighted in gray, (III) grain size chart. Black areas represent pixels with CI < 0.1 that have not been included, yellow regions are from the bare silicon wafer and grain boundaries are represented in white in the IPF maps. All IPFs and IPF maps are of the sample normal direction (001).

Figure S26. EBSD scans of (I) HOPG-A (Optigraph), (II) HOPG B (Optigraph) and (III) HOPG B (XFNano): (i) IPF map, (ii) unique grain color map, (iii) grain size chart, (iv) IPF and, (v) (0001) and (1011) PFs. Black areas represent pixels with CI < 0.1 that have not been included, grain boundaries are represented in gray and yellow regions are from the bare silicon wafer in the IPF maps. The points in the PFs and IPFs have been weighted by grain size. All IPFs and IPF maps are of the sample normal direction (001).

Sample Details	Step size	ISR (%)	Largest grain size	
	(µm)		Diameter (µm)	Area (µm ²)
HOPG A	4	83	26	1066
(Optigraph)				
HOPG B	1	55	13	140
(Optigraph)				
HOPG B	1.2	92	32	820
(XFNano)				

Table S6: Details of EBSD scans of HOPG

Figure S27. EBSD scan of a silicon wafer with the input phase as (I) Silicon: (i) IPF map, (ii) (001) PF, and, (iii) IPF; (II) Graphite: (i) IPF map, (ii) (0001) and $(10\overline{1}1)$ PFs, and, (iii) IPF. Grain boundaries are in white. All IPFs and IPF maps are of the sample normal direction (001).

XRD Characterization of Graphite Films

Sample Details	2θ (°)	FWHM (°)	FWHM (°)- corrected	d0002 (Å)
Grade A HOPG (Optigraph)	26.522	0.168	0.103	3.358
Grade B HOPG (Optigraph)	26.455	0.218	0.173	3.667
Grade A HOPG (SPI)	26.482	0.223	0.180	3.363
Grade B HOPG (XFNANO)	26.557	0.192	0.138	3.353
Sample A (inner)-8-8- 18-E (type B)	26.568	0.201	0.151	3.352
Sample B (outer)-4-2- 19-C (type B)	26.551	0.200	0.149	3.354
8-2-18-US-A (type B)	26.560	0.163	0.094	3.352
8-2-18-DS-B (type B)	26.561	0.203	0.153	3.353
4-4-19-A (type B)	26.554	0.173	0.111	3.354
3-27-19-D (type B)	26.561	0.200	0.149	3.353
4-4-19-F (type B)	26.571	0.188	0.133	3.352
Sample 1 (wrinkled)- (type A)	26.571	0.188	0.133	3.352

<u>**Table S7-(i)**</u>: Lattice spacing for d_{002} from XRD with Cu-K α radiation and a 0-D detector.

A FWHM of 0.133° was obtained for $2\theta = 41.780^{\circ}$ for Sapphire-0001 and was used to correct for instrumental broadening. Generally, for HOPG like materials the crystal sizes are too large (> 1 μ m) to be determined by the Scherrer equation.⁹⁻¹¹

Mosaic spread may be determined by varying or 'rocking' the incident beam relative to the Bragg

angle of interest.

Sample Details	θ (°)	Mosaic Spread (°)
Grade A HOPG (Optigraph) ¹	27.369	0.533
Grade B HOPG (Optigraph) ¹	27.340	0.963
Grade A HOPG (XFNANO) ¹	27.292	0.775
Grade B HOPG (XFNANO) ²	26.697	0.887
Sample A-8-8-18-E (type B)	27.332	0.210
8-2-18-DS-B (type B)	27.327	0.238
8-2-18-US-A (type B)	27.309	0.093
4-4-19-F (type B)	27.297	0.115
Sample 1 (wrinkled) ³ - (type A)	27.279	0.551
Sample 1 (wrinkled) ³ -pressed-	27.305	0.377
(type A)		

<u>Table S7-(ii)</u>: Mosaic spreads from Rocking Curve Experiments around the (004) peak at $2\theta = 54.66^{\circ}$

¹Sample thickness ~1000 μ m; ²Sample thickness ~ 1–2 μ m; ³Sample thickness ~250 nm. All other sample thicknesses ~ 800 nm.

The mosaic spreads have not been corrected for instrumental broadening. However, on running the same measurement for single crystal c-sapphire, the 20.61° theta peak gave a value of 0.0481°, indicating that an inherent instrumental broadening is present. Thickness variations and curvature (i.e. the fact that the films are not perfectly flat on the silicon wafer) are also expected to contribute to the mosaic spread.¹²

<u>*H*₂ pre-treatment of Ni</u>

The first part of all Type A and Type B processes included a H₂ pre-treatment step (step 1, **Figure** 1). In addition to cleaning the Ni surface from surface oxides, considerable grain growth was observed, with larger average grain sizes with increasing temperature.

Figure S28. Schematic of the H₂ pre-treatment step reproduced to determine Ni grain size.

Table S8.	Ni grain	sizes	after	H_2	pre-treatment a	t 1150	°C
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Conditions	Largest grain	Average grain
	diameter (µm)	diameter (µm)
As received Ni-100	8	2
Ni-100	846	470
Ni-25	130	61

Figure S29. EBSD of Ni: (I) As-received Ni, (II) after H_2 pre-treatment at 1150 °C; (i) IPF map, (ii) grain size chart, (iii) (001) PF, and, (iv) IPF. Black areas represent pixels with CI < 0.1 that have not been included and grain boundaries are represented in white in the IPF maps. All IPFs and IPF maps are of the sample normal direction (001).

Graphite Films from 25 µm thick Ni foils

Graphite films with smaller grains were obtained under the same process conditions (Process B) with the largest grain sizes ~ 0.24 mm.

Figure S30. Ni after H_2 pre-treatment at 1150 °C: 25 µm Ni (i) IPF map, (ii) grain size chart, (iii) (001) PF, and, (iv) IPF. Black areas represent pixels with CI < 0.1 that have not been included and grain boundaries are represented in gray in the IPF maps. All IPFs and IPF maps are of the sample normal direction (001).

Figure S31. EBSD scan of a Type B 'collapsed' graphite film synthesized on a 25 μ m Ni foil. (I) IPF map (scale bar: 500 μ m), (II) Grain size chart, (III) (0001) and (1011) PFs, and, (IV) IPF. Grain boundaries are shown in white, black areas represent pixels with CI < 0.1 that have not been included and yellow regions are from the bare silicon wafer in the IPF maps. The points circled in yellow on the IPFs and PFs are from the bare silicon wafer. The points in the PFs and IPFs have been weighted by grain size. All IPFs and IPF maps are of the sample normal direction (001).

<u>**Table S9**</u>: Details of EBSD scans from graphite films synthesized on 25 μ m Ni foils

Sample Details	Step size (µm)	ISR (%)	Largest grain size	
			Diameter (µm)	Area (µm ²)
Graphite (Ni-25 μm) Fig. S31	25	63	240	90538

Figure S32. Typical EELS spectrum showing the absence of chlorine and the presence of sp² hybridized C, from the cross-section of a Type B graphite film.

Mechanical property calculations

Effect of wrinkles: The increase in in-plane stiffness may be estimated using reference [13] for a film of thickness T from which wrinkles, having an amplitude A that is small compared to their mean separation distance and occupying an area fraction f, have been removed. We have accordingly found that $E_{(f=0)}/E_{(f)}=1+k*f*(A/T)^2$, where k=6 is a theoretical value and $E_{(f=0)}$ and $E_{(f)}$ represent the Young's modulus of the wrinkle-free and wrinkled films respectively.¹³ Thus, for example, removing a 0.1 (=f) area fraction of wrinkles for films that have (A/T) ranging from 1–10 would increase the Young's modulus by a factor of 0.6–60. Removal of wrinkles is not expected to significantly influence the strength.

Effect of grain size on film strength: In general, the tensile strength s of the film is determined from the size m (in terms of atomic size) of its largest defects as $s(m) = s(m=0)*(1+m)^{-n}$, with 0<n<1. An intermediate value of n=1/2 is theoretically predicted for this equation from quantized fracture mechanics^{14,15} (whereas other values could describe nonlinear constitutive laws, re-entrant corner defects, or the weakest link theory).

<u>Hall-Petch like behavior</u>: Considering the defect size m=c1*d, and thus proportional via a constant c1 to the grain size d, would result in the well-known Hall-Petch law, i.e. $s(d)=s(d=0)*(1+c1*d)^{-n}$ with n=1/2. Again, the constant c1 is the inverse of a characteristic length. Thus, s(d) is nearly proportional to d⁻ⁿ. The direct Hall-Petch-like law has been observed in silico via molecular dynamics (MD) simulations for polycrystalline graphene by Song et. al.,¹⁶ with s(d=0)=62 GPa suggesting that smaller grain size is beneficial for the strength up to this last value, that could thus be interpreted as the strength of amorphous graphene. However, the full removal of grain boundaries and the recovering of the crystalline nature of graphene could further increase the strength to the graphene ideal strength of about 100GPa (for example, 98GPa or 115GPa are the values reported along the armchair and zigzag directions respectively¹⁶).

<u>Inverse Hall-Petch like behavior</u>: Another intepretation is to consider the defect size as proportional to the number of grain boundary (GB) junctions, which geometrically is proportional to d^{-2} , so that $s(d)=s(d=\infty)^*(1+c2/d^2)^{-n}$ where c2 is a constant. Thus, s(d) is nearly proportional to d^{2n} , representing an inverse Hall-Petch law. The inverse Hall-Petch law has been observed in silico by MD simulations for polycrystalline graphene by Sha et. al.,¹⁷ with s(d)=31GPa/nm^0.1*d^0.1, verifying also that the scaling of the number or density of GB junctions is proportional to d^{-2} .

Using this last strength scaling equation, we can quantify the strengthening due to the removal of GBs, assuming that they are the weakest links observed experimentally.¹⁷ Thus, the strength increase in a graphite film of size L that results from an increase in grain size from a size d to a single crystal of size L may be roughly estimated as: $s(d=L)/s(d)=(L/d)^{0.1}$. For example, the strength increases by a factor of ~2 if L/d changes from 10000–10.

Effect of grain size on film stiffness. The same power law type of scaling has been observed by both Song et. al. and Sha et. al. ^{16, 17} for Young's modulus, suggesting film stiffenning by GB removal. Accordingly, the potential applications for both wrinkle-free and grain boundary-free graphite films are where "high modulus and high strength carbon films" are required.

Figure S33. Schematic depicting a possible route for the formation of Type B graphite film in steps 3 and 4 (as described in **Figure 1**).

The schematic above takes the following observations into account: (1) the etching started from the edges of the Ni foils and proceeded inward such as in **Figure S8-(ii)**, and (2) a Ni foil with an area $\sim 1 \text{ cm}^2$ formed 2 graphite films (on its top and bottom surfaces) with $\sim 1 \text{ cm}^2$ lateral areas. The surface of the graphite film that was originally in contact with the Ni foil substrate has been referred to as the 'inner' surface and the opposite surface as the 'outer' surface. Thus, as per the above schematic, regions closer to the outer surface were formed during step 3, while regions closer to the inner surface were formed during step 3, while regions closer to the inner surface were formed to suffer to silicon wafers such that either the inner or the outer surface was exposed and thus, the surface studied. No obvious differences have been observed between the outer and the inner surfaces (from similarly synthesized different films) in terms of graphite quality, using multiple characterization techniques. Examples include:

1. EBSD scans: **Figures 4-I** and **4-II** are, respectively, from the inner and outer surfaces of two different graphite films.

2. Raman maps:

Table S3-(i): Samples 1-2: inner surface; Samples 3-4: outer surfaceTable S3-(ii): Samples B-C: inner surface

3. XRD: As explained in the main text, the entire thickness of the film is interrogated by XRD.
Table S7-(i): Sample A:inner surface, Sample B:outer surface
Table S7-(ii): Sample A-8-8-18-E: inner surface, 8-2-18-US-A: outer surface

HR-TEM and EELS Analysis: HR-TEM and EELS have been used to study and explore graphitization in cross-section TEM samples. No obvious differences were observed in terms of graphite quality between the top and middle regions (**Figure S34**) from HR-TEM imaging.

Figure S35 shows EELS spectra collected at ~20 nm intervals from a cross-section sample. For the C-K edge, the maximum π^*/σ^* intensity was observed close to the 'inner' surface of the film, implying that the highest quality graphite might be contained in this region. In any case, we note that the variation is relatively small, and the sample is "well graphitized" throughout the entire cross section. (Please note that variations in quality in cross-section TEM samples may also arise from exposure to ion or electron beams during sample preparation or imaging).

Figure S34. HR-TEM images of a cross-section sample: (i) image, and (ii) electron diffraction pattern; images from (iii) top region, and, (iv) middle region; (v) is a higher magnification image of the middle region with its digital diffractogram pattern shown in the inset. Scale bars for (iii)-(v): 10 nm.

Figure S35. (i) Image of a cross-section sample; (ii)-(iii): corresponding EELS spectra.

Oxygen Plasma Etching: Oxygen plasma etching has been used to etch and compare samples through EBSD. Two plasma strengths were used, ST1 resulted in the etching of about 80 to 100 nm, while ST2 resulted in the etching of about 40 to 50 nm. As the upper graphene layers are etched away, similar layers lying underneath are revealed.

Figure S36-I. IPF maps of the sample normal direction (001) from EBSD scans of a plasma etched Type B film with the 'outer' surface exposed: (i) 1 h (etched by about 60 to 75 nm), (ii) 3 h (about 140 to 175 nm etched). Grain boundaries are represented in white, black areas represent pixels with CI < 0.1 that have not been included and yellow regions are from the bare silicon wafer.

Figure S36-II. IPF maps of the sample normal direction (001) from EBSD scans of a plasma etched Type B film with the 'inner' surface exposed: (i) 0 min, (ii) 50 min, (iii) 1 h 50 min, (iv) 4 h (about 160 to 200 nm). Grain boundaries are represented in white, black areas represent pixels with CI < 0.1 that have not been included and yellow regions are from the bare silicon wafer.

However, as oxygen plasma etching is a destructive technique, a reduction of grain size was observed (**Figure S37-I**). Again, 3-4 h (up to 200 nm) of etching resulted in surface roughening (**Figure S37-II**) and the appearance of a prominent D peak (**Figure S37-III**). Similar surface roughening and the appearance of a D peak were observed after plasma etching grade A HOPG (**Figure S38**).

Figure S37-I. Grain size reduction with oxygen plasma etching: (i) 1 h, and, (ii) 3 h.

Top: IPF maps of the sample normal direction (001) with the largest grain highlighted in gray; grain boundaries are represented in white, black areas represent pixels with CI < 0.1 that have not been included and yellow regions are from the bare silicon wafer. Bottom: grain size charts with the largest grains highlighted in gray.

Figure S37-II. SEM images of Type B films film etched for 3- 4 h (about 200 nm) with oxygen plasma, scale bars: (i) 1 mm, (ii) 100 μ m, (iii) 10 μ m, (iv) 5 μ m.

Figure S37-III. Typical Raman spectrum of a Type B film etched for 3-4 h (about 200 nm) with oxygen plasma.

Figure S38. An oxygen plasma etched grade A HOPG sample: (i) Raman spectrum after 30 min (about 40-50 nm), (ii) SEM image after 1 h (about 80-100 nm).

Please note that mechanical exfoliation methods (using sticky notes, scotch-tape, carbon tape or transfer tapes) were found, in our hands, to be mostly un-suitable. This was because of the poor adhesion of the films to the silicon substrates; the films would transfer to the adhesive surfaces in their entirety. Also, mechanical damage to the films were possible, making it difficult to reach conclusions about the new surfaces now revealed. Attempts to explore the flakes on the adhesive tapes also proved to be difficult, including keeping track of exactly what depth of the film these new flakes were from and the requirement to transfer such new flakes to flat surfaces (like silicon wafers) on which EBSD and other characterization would be possible. Our efforts as described above suggest to us that new methods (inventing new methods) would seem to be helpful for preparing "sections" of graphite film samples.

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